

Fall 2017

CSCI 420: **Computer Graphics**

13.2 Physically Based Simulation II

Mass-Spring Systems



Hao Li

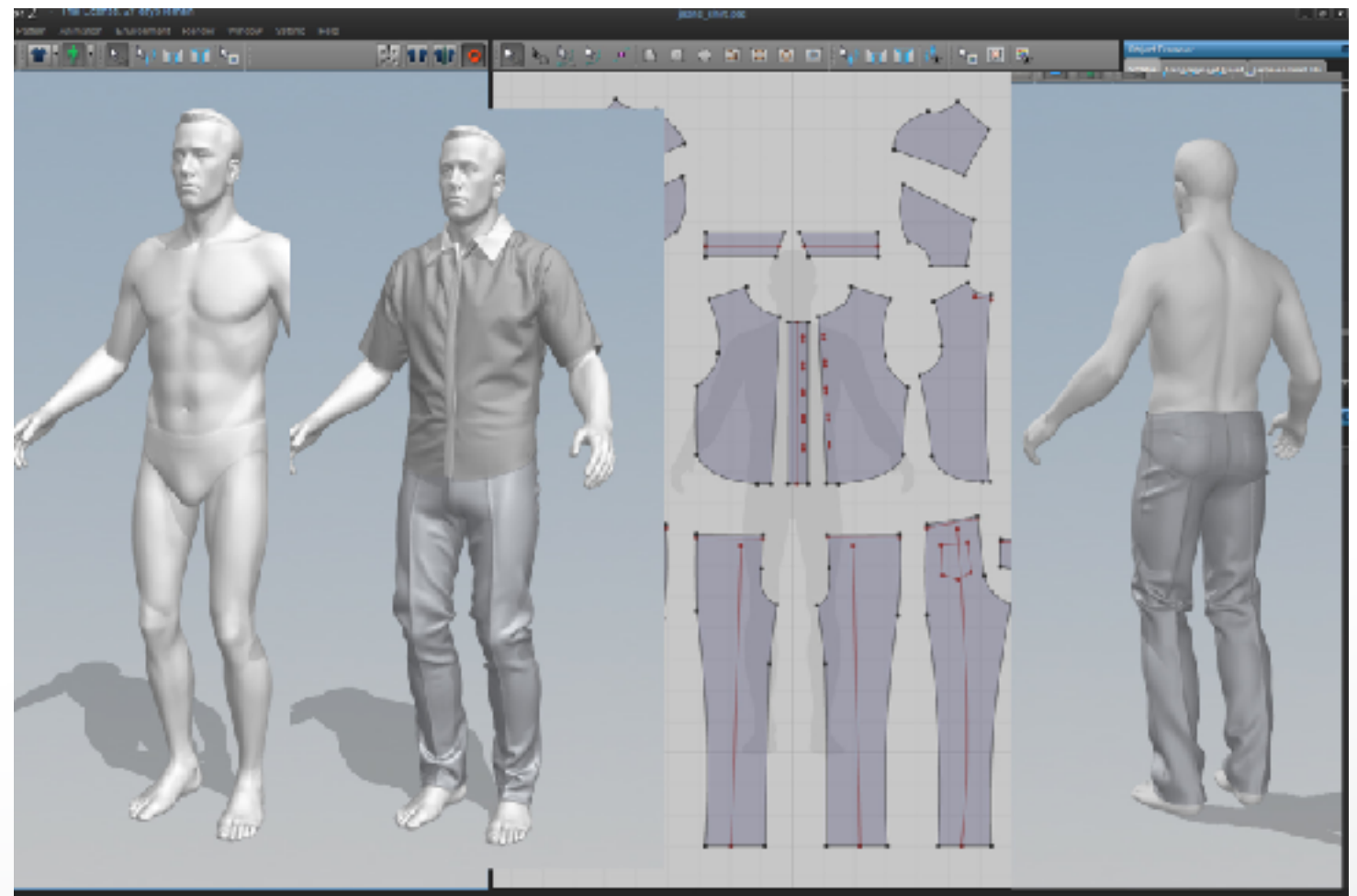
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Mass-Spring Systems

- **The 101 of Physics Simulation**
- What do we want to simulate? **Deformable Objects**
- Design a model. **Mass points + springs.**
- Write differential equations. **Newton's 2nd Law (Hooke)**
- Discretize equations. **Integration methods for ODEs**
- Add interaction. **Collision detection + response**
- Simulate!

Mass-Spring Systems

- Simulation of cloth based on deformable surfaces (Polygonal mesh)
- Realistic simulation of cloth with different fabrics such as wool, cotton, or silk for garment design



Facial Animation

- Simulation of facial expressions based on deformable surfaces/volumes/muscles
- Animation of face models from speech and mimic parameters

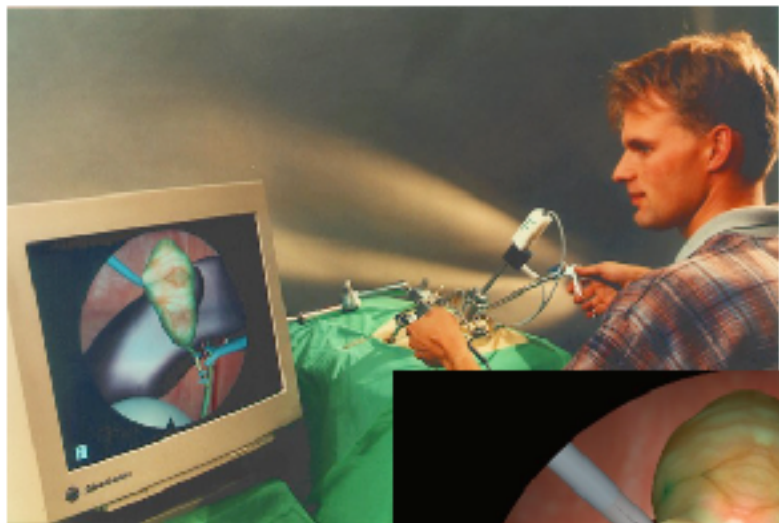


Thalmann

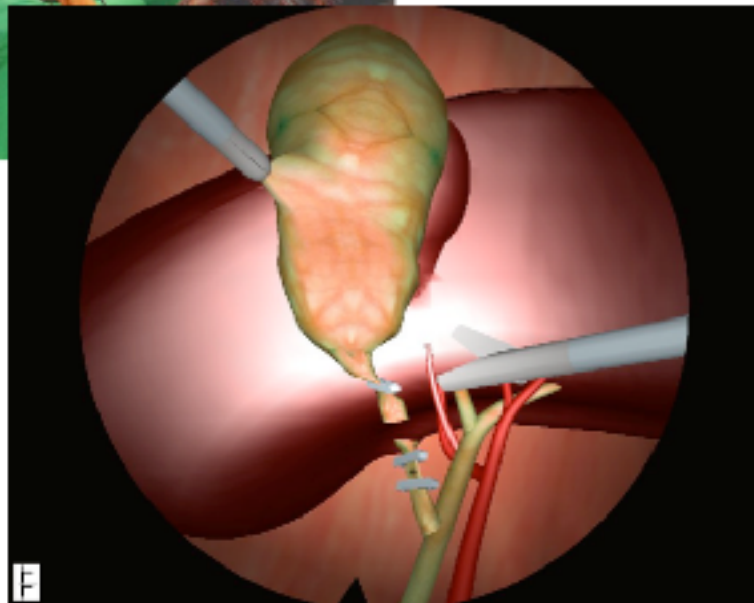


Medical Simulation

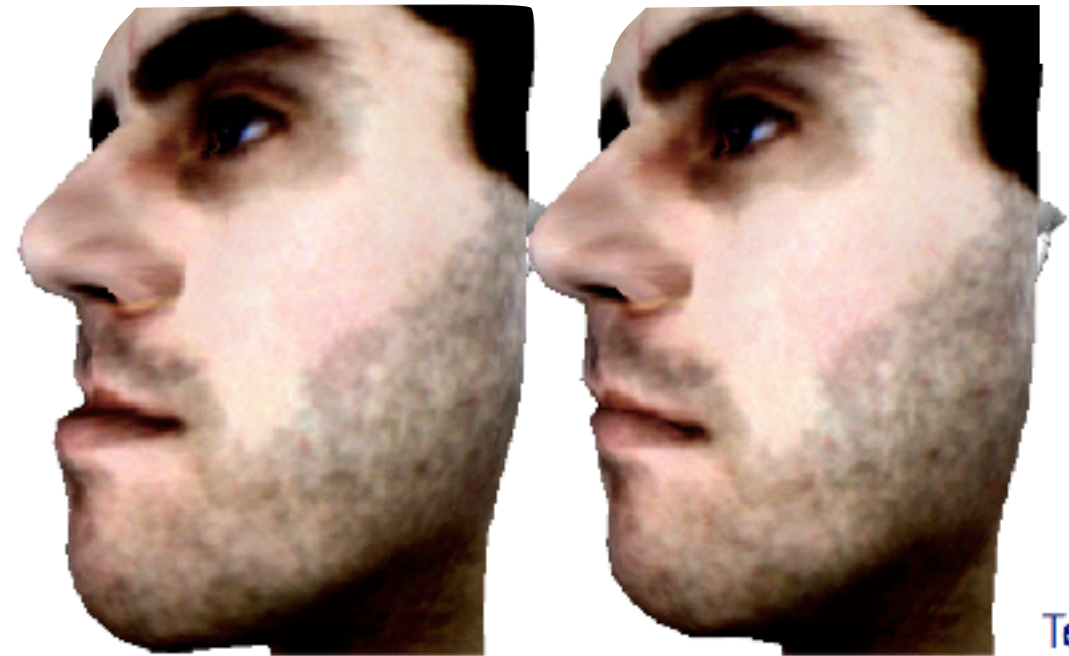
- Simulation of deformable soft tissue
- Surgical planning
- Medical training



Virtual
endoscopy



Kuehnappel



Teschner

Prediction of the surgical outcome
in craniofacial surgery

Overview

- Model and Physics
- Implementation Hints
- Time-Discretization
- Collision Response
- (Simulation Loop)

Mass-Point System

- Discretization of an object into mass points (gas, fluid, elastic object, inelastic object)
- System with multiple mass centers (Planetary System)
- Interaction between points i and $j \neq i$ based on internal forces $\mathbf{F}_{ij}^{\text{int}}$
- All other forces at point i are external forces $\mathbf{F}_i^{\text{ext}}$
- Overall force $\mathbf{F}_i = \mathbf{F}_{ij}^{\text{int}} + \mathbf{F}_i^{\text{ext}}$

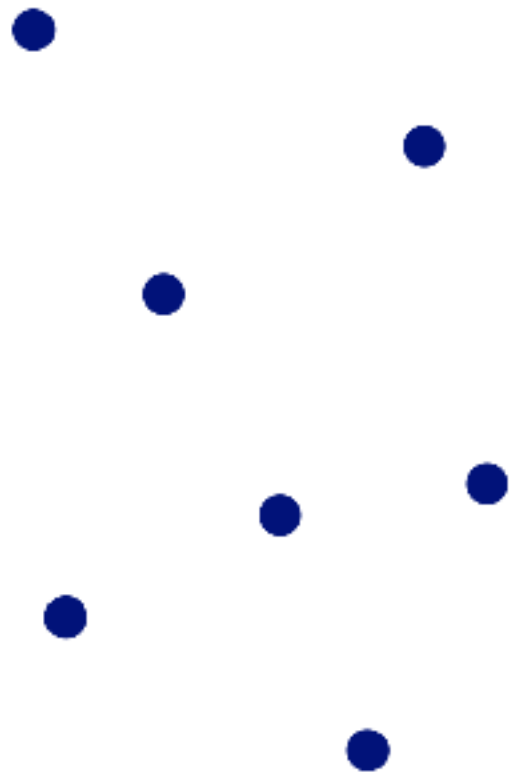
$$\mathbf{F}_{ij}^{\text{int}} = -\mathbf{F}_{ji}^{\text{int}}$$

$$\sum_i \sum_j \mathbf{F}_{ij}^{\text{int}} = 0$$

Mass-Point System

- Discretization of an object into mass points
- Representation of forces between masses by springs
- Computation of dynamics

Mass-Points



Object sampled using mass points

Mass of object: M

Number of points: n

Mass of each point: $m = M/n$

(if uniformly distributed)

Simulate the motion of each mass point

Physically-based Equations

Equations that describe the behavior of the system (i.e. the mass points)

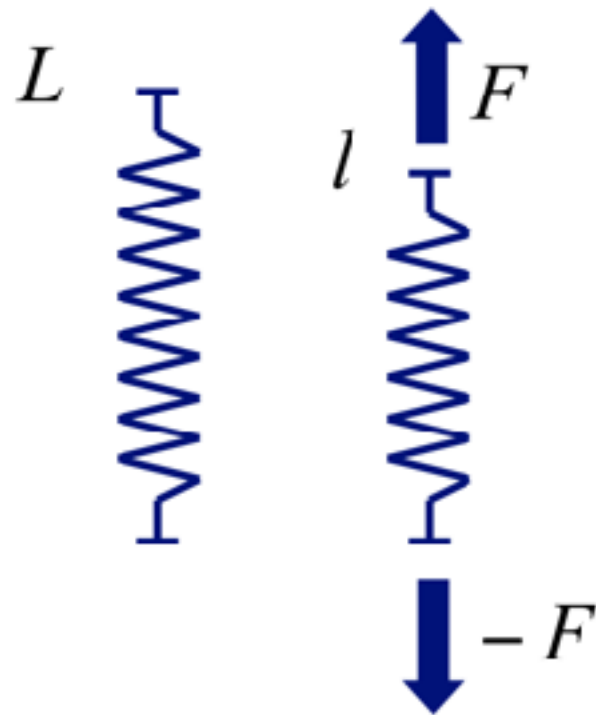
Physically-based model:

Newton's 2nd Law

$$\sum \mathbf{F}_i^{\text{int}} + \mathbf{F}_i^{\text{ext}} = m\mathbf{a}_i$$

Next: Model the forces

Elastic Forces: Springs



Spring stiffness is denoted as k

Initial spring length L

Current spring length l

Deformation linear w.r.t. force:

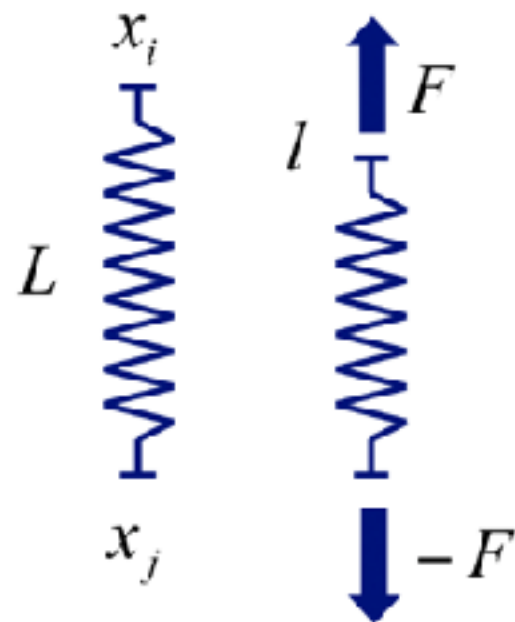
$$F = -k(l - L)$$

Hooke's
Law

Elasticity: Ability of a spring to return to its initial form when the deforming force is removed.

Simple mechanism for internal forces.

Elastic Energies



Elastic energy:

$$E = \frac{1}{2} k (l - L)^2$$

Force = - Partial Derivative (Gradient)

$$F_i = - \frac{\partial E}{\partial x_i}$$

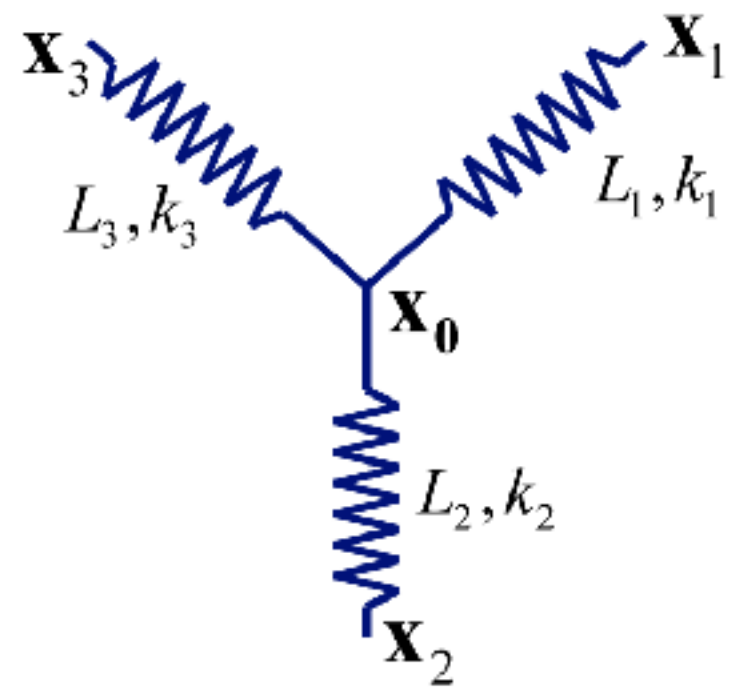
Force in vector notation:

$$\mathbf{F}_i = -k(l - L) \frac{\mathbf{x}_i - \mathbf{x}_j}{l}$$

Force-centered view versus energy-centered view

Forces at a Mass Point

Internal forces \mathbf{F}^{int}



External forces \mathbf{F}^{ext}

Gravity

Contact forces

All forces that are
not caused by springs

Resulting force at point i

$$\mathbf{F}_0^{\text{int}} = - \sum_{i \in \{1,2,3\}} k_i (l_i - L_i) \frac{\mathbf{x}_i - \mathbf{x}_0}{l_i}$$

$$\mathbf{F}_i = \mathbf{F}_i^{\text{int}} + \mathbf{F}_i^{\text{ext}}$$

Dissipative Forces

Dissipative forces

Damping
Friction

$$\mathbf{F}^{damping}(t) = -\gamma \cdot \mathbf{v}(t)$$

System Equations

Equation of Motion for one mass point (3 eqs.)

$$m_i \frac{d^2 \mathbf{x}_i(t)}{dt^2} = \mathbf{F}_i^{\text{int}}(t) + \mathbf{F}_i^{\text{ext}}(t)$$

Equation of Motion for a system of mass points (3n eqs.)

$$\mathbf{M} \frac{d^2 \mathbf{X}(t)}{dt^2} = \mathbf{F}^{\text{int}}(t) + \mathbf{F}^{\text{ext}}(t)$$

M is a diagonal matrix

System Equations

Incorporation of **damping**

$$\mathbf{M} \frac{d^2 \mathbf{X}(t)}{dt^2} + \mathbf{D} \frac{d\mathbf{X}(t)}{dt} = \mathbf{F}^{\text{int}}(t) + \mathbf{F}^{\text{ext}}(t)$$

Overview

- Model and Physics
- Implementation Hints
- Time-Discretization
- Collision Response
- (Simulation Loop)

Elastic Spring

```
class SPRING
{
    public:
        POINT *point1;
        POINT *point2;
        float stiffness;      // k
        float initialLength; // L
        float currentLength; // l

        . . .
}
```


Mass Point

```
class POINT
{
    public:
        float mass;
        float position[3];
        float velocity[3];
        float force[3];
        float damping;

        . . .
}
```

Force Computation

```
for all points
    point_i.ClearForce()
    point_i.AddGravityForce()

//Add other external forces

for all springs
    spring_i.ComputeElasticForce()
    spring_i.AddForceToEndPoints()
```

Overview

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- Time-Discretization
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System Equations

System of $3n$ 2nd order Ordinary Differential Equations (ODE)

$$\mathbf{M} \frac{d^2 \mathbf{X}(t)}{dt^2} + \mathbf{D} \frac{d\mathbf{X}(t)}{dt} = \mathbf{F}^{\text{int}}(t) + \mathbf{F}^{\text{ext}}(t)$$

One 2nd order ODE (1-dimensional problem)

$$m \frac{d^2 x(t)}{dt^2} + \gamma \frac{dx(t)}{dt} = F(t)$$

Initial value problem: $x(0)$ and $v(0)$ are known

Solution

- a) Analytical solution (if we care about the exact state at time t)
- b) **Discrete** solution
 - Graphics: the goal is to **display** the state at t_i
 - Find solution at discrete time instants t_i , assuming that we know previous solutions t_{i-1} , t_{i-2} , etc.
 - We do not care about the steady state error, but we want **plausible behavior** and **response to external forces**

Problem

- We have:
 - Initial position \mathbf{x}
 - Initial velocity \mathbf{v}
 - 2nd derivative of position \mathbf{x} with respect to time

$$\frac{d^2 \mathbf{x}_i(t)}{dt^2} = \frac{\mathbf{F}_i(t) - \gamma \mathbf{v}_i(t)}{m_i}$$

- **Goal:** Computation of position \mathbf{x} over time

Numerical Integration Methods

- Explicit Integration
 - Euler
 - Leapfrog
 - Heun
 - Midpoint
 - Runge-Kutta methods
- Implicit Integration
 - Backward Euler
- Predictor-Corrector methods
 - Gear
- Methods for higher order ODEs
 - Verlet
 - Beeman
- Variable time-step methods

Numerical Integration Methods

- Reduction of a second-order ODE to two coupled first-order ODEs.

$$m_i \frac{d^2 \mathbf{x}_i(t)}{dt^2} + \gamma \frac{d\mathbf{x}_i(t)}{dt} = \mathbf{F}_i$$

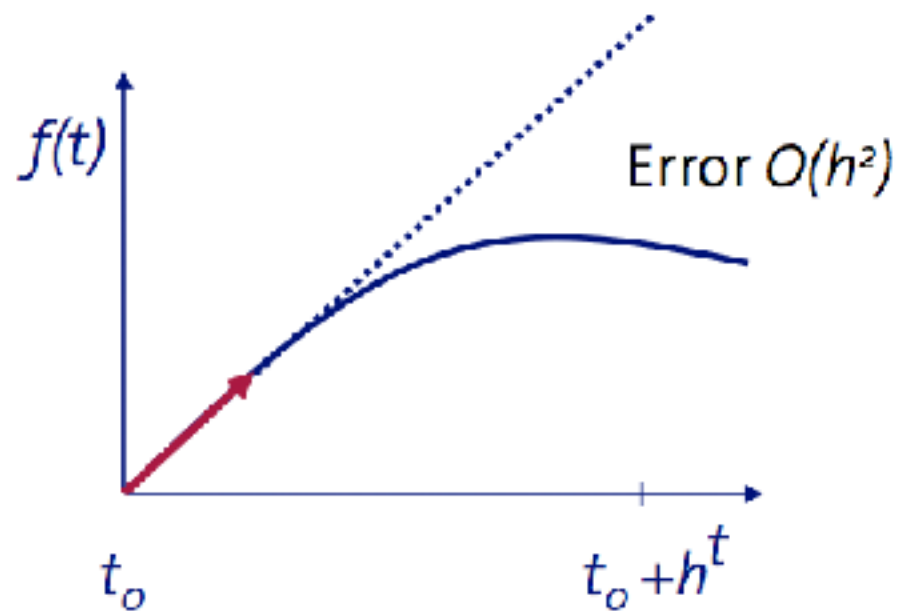


$$\frac{d\mathbf{x}_i(t)}{dt} = \mathbf{v}_i(t) \quad \frac{d\mathbf{v}_i(t)}{dt} = \frac{\mathbf{F}_i(t) - \gamma \mathbf{v}_i(t)}{m_i}$$

velocity

acceleration

Explicit Integration



- Initial value $f(t_0)$
- Compute the derivative at t_0
- Move from t_0 to $t_0 + h$ using the derivative at t_0

Euler Method

Leonard Euler:
1707 (Basel) – 1783 (St. Petersburg)

Explicit Integration

$$f(t_0 + h) = f(t_0) + h \cdot f'(t_0) + \frac{h^2}{2} f''(t_0) + \dots$$

Taylor series

$$f(t_0 + h) = f(t_0) + h \cdot f'(t_0) + O(h^2)$$

$$f(t_0 + h) \cong f(t_0) + h \cdot f'(t_0)$$

Euler method

Explicit Integration

$$\mathbf{x}'(t) = \mathbf{v}(t) \quad \mathbf{v}'(t) = \frac{\mathbf{F}(t) - \gamma \mathbf{v}(t)}{m}$$

Start with initial values	$\mathbf{x}(t_0) = \mathbf{x}_0 \quad \mathbf{v}(t_0) = \mathbf{v}_0$
Compute	$\mathbf{v}'(t_0) \quad \mathbf{x}'(t_0)$
Assume	$\mathbf{v}'(t) = \mathbf{v}'(t_0) \quad \mathbf{x}'(t) = \mathbf{x}'(t_0) \quad t_0 \leq t \leq t_0 + h$
Compute	$\mathbf{x}(t_0 + h) = \mathbf{x}(t_0) + h\mathbf{x}'(t_0) = \mathbf{x}(t_0) + h\mathbf{v}(t_0)$
Compute	$\mathbf{v}(t_0 + h) = \mathbf{v}(t_0) + h\mathbf{v}'(t_0) = \mathbf{v}(t_0) + h \frac{\mathbf{F}(t_0) - \gamma \mathbf{v}(t_0)}{m}$

$\mathbf{F}(t)$ is computed from $\mathbf{x}(t)$ and external forces!

Error Accumulation

$$\mathbf{x}'(t) = \mathbf{v}(t) \quad \mathbf{v}'(t) = \frac{\mathbf{F}(t) - \gamma \mathbf{v}(t)}{m}$$

Euler step from t_0 to t_0+h

$$\mathbf{x}(t_0 + h) = \mathbf{x}(t_0) + h\mathbf{v}(t_0) \quad \mathbf{v}(t_0 + h) = \mathbf{v}(t_0) + h \frac{\mathbf{F}(t_0) - \gamma \mathbf{v}(t_0)}{m}$$

$$\mathbf{x}(t_0 + 2h) = \mathbf{x}(t_0 + h) + h\mathbf{v}(t_0 + h)$$

Euler step
from t_0+h to t_0+2h

$$\mathbf{v}(t_0 + 2h) = \mathbf{v}(t_0 + h) + h \frac{\mathbf{F}(t_0 + h) - \gamma \mathbf{v}(t_0 + h)}{m}$$

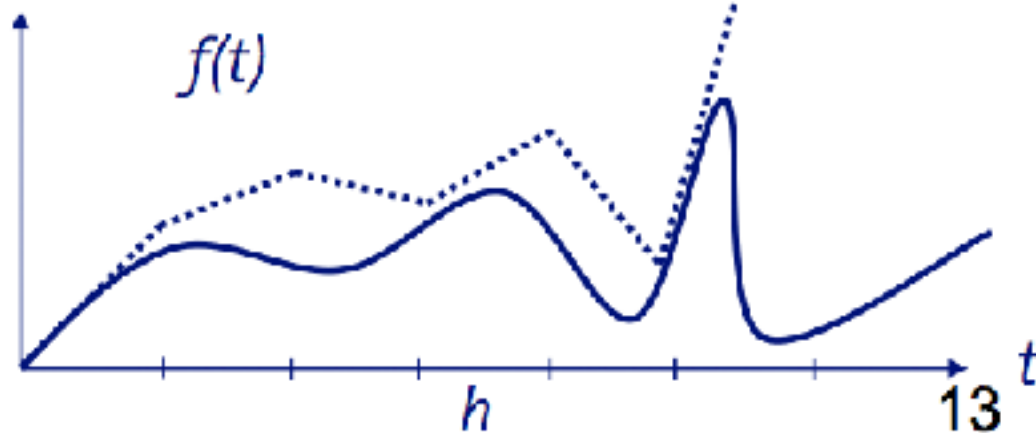
Problems

- Numerical integration is inaccurate.

$$\underbrace{f(t+h) = f(t) + f'(t)h}_{\text{Euler step}} + \boxed{O(h^2)}$$

Error

- Inaccuracy can cause instability.



Error

$$0 \leq e < \frac{h^2}{2} \cdot f''(t_e), \quad t_e \in [t, t+h]$$

Improving Accuracy - Leap Frog

$$\mathbf{v}(t + h/2) = \mathbf{v}(t - h/2) + h \cdot \mathbf{a}(t)$$

$$\mathbf{x}(t + h) = \mathbf{x}(t) + h \cdot \mathbf{v}(t + h/2)$$

Error $O(h^3)$

time step h is significantly larger compared to Euler

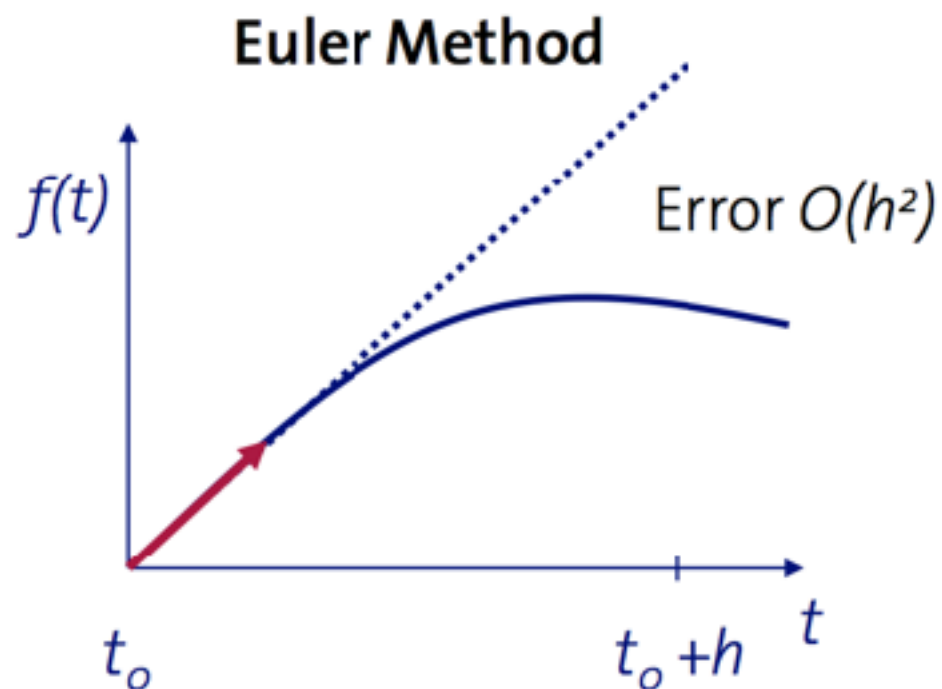
Implementation

Euler	Leapfrog
<pre>... addForces(); // F(t) positionEuler(h); // x=x(t+h)=x(t)+hv(t) velocityEuler(h); // v=v(t+h)=v(t)+ha(t) ...</pre>	<pre>initV() // v(o) = v(o) - h/2a(o) ... addForces(h); // F(t) velocityEuler(h); // v=v(t+h)=v(t)+ha(t) positionEuler(h); // x=x(t+h)=x(t)+hv(t+h) ...</pre>

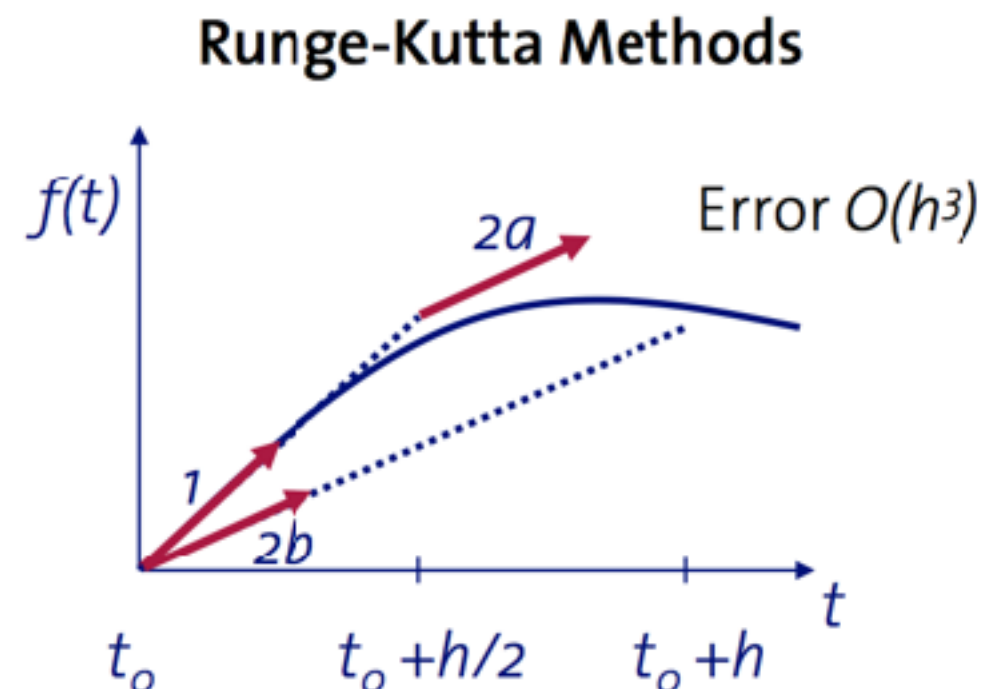
(In practice, it is irrelevant that velocities are computed at mid time steps)

Improving Accuracy - Runge Kutta

2nd order (midpoint method)

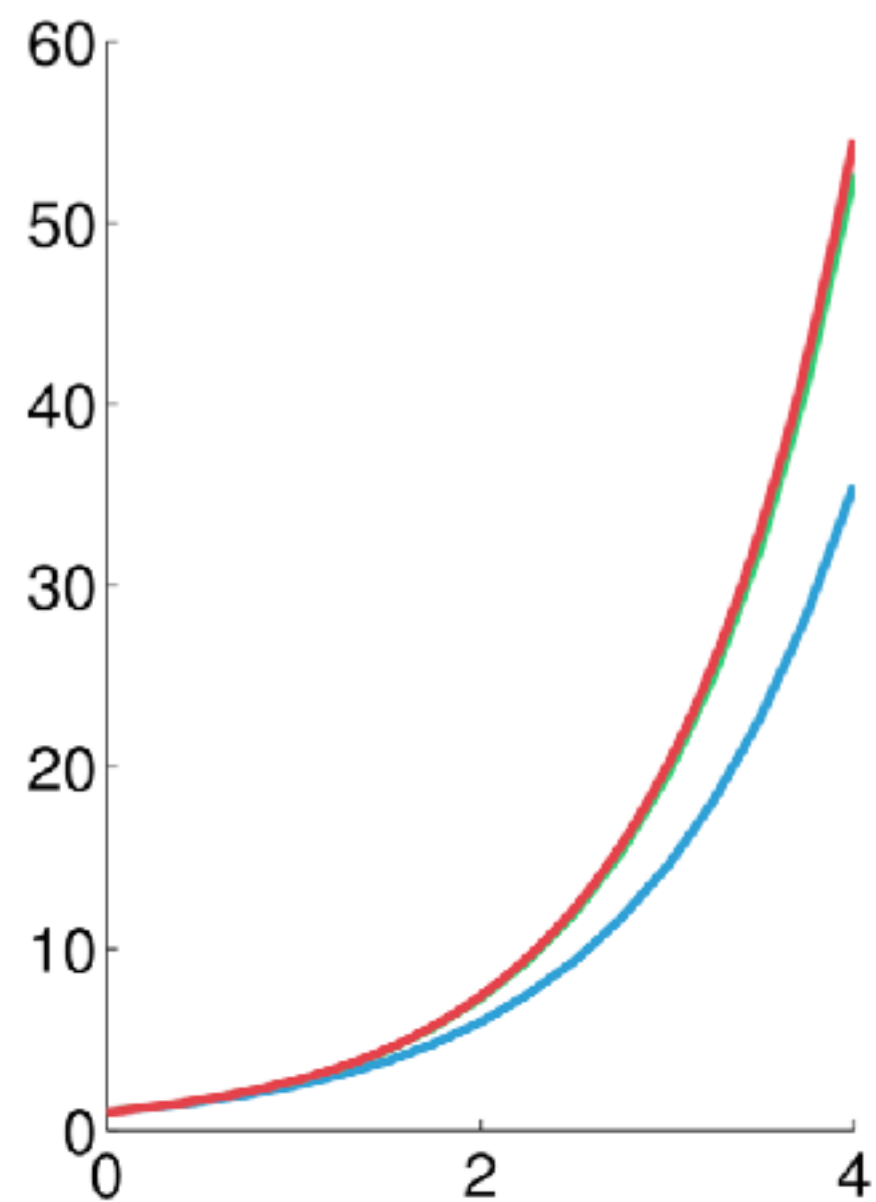
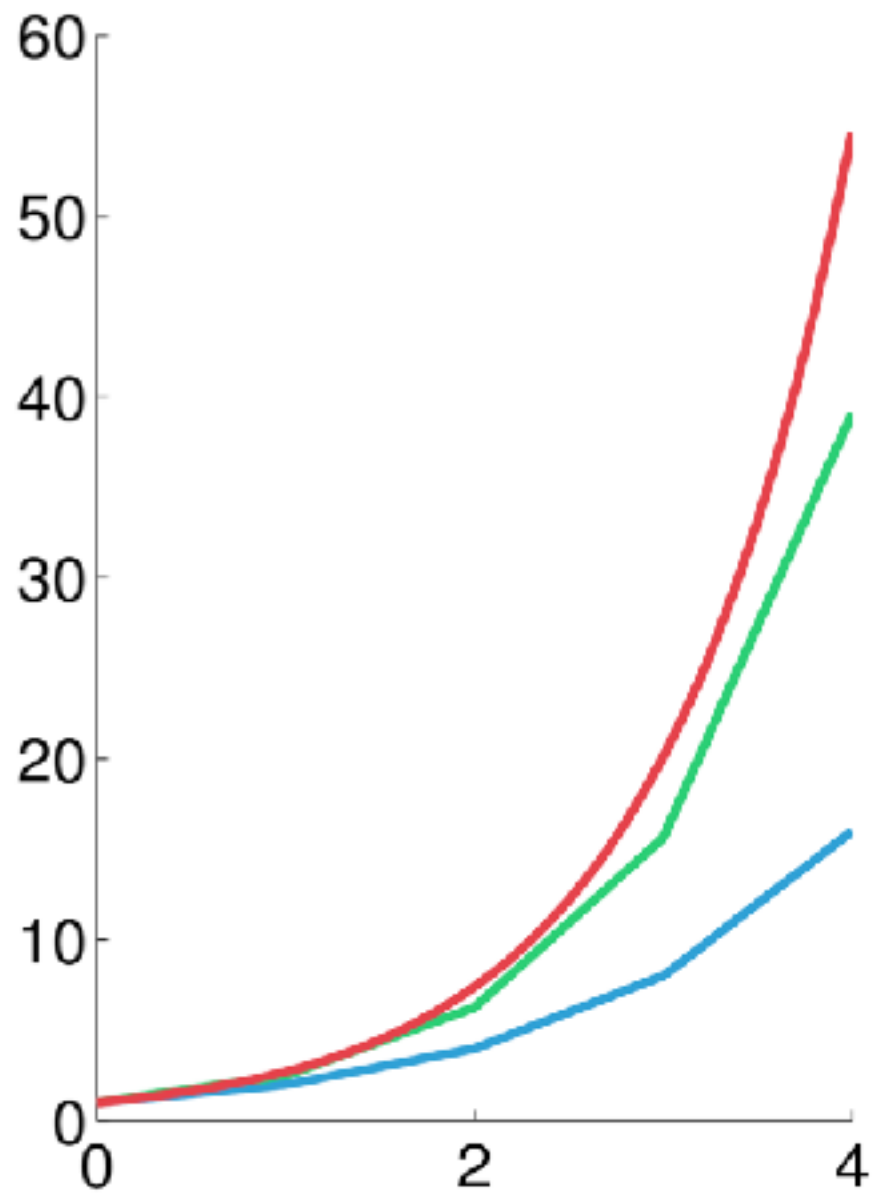


- Compute the derivative at t_0
- Move from t_0 to t_0+h using the derivative at t_0



- Compute the derivative at t_0
- Move to $t_0+h/2$
- Compute the derivative at $t_0+h/2$
- Move from t_0 to t_0+h using the derivative at $t_0+h/2$
- Second order R-K also called "midpoint"

Midpoint vs Euler



- Green = Midpoint
- Blue = Euler
- $h=1$ vs. $h=1/4$

Implementation

Euler Method

Straightforward:

- Compute spring forces
- Add external forces
- Update positions
- Update velocities

Runge-Kutta Methods

- Compute spring forces
- Add external forces
- Compute **auxiliary** positions and velocities
 - once for second-order
 - three times for fourth-order
 - requires **additional data copies**
- Update positions
- Update velocities

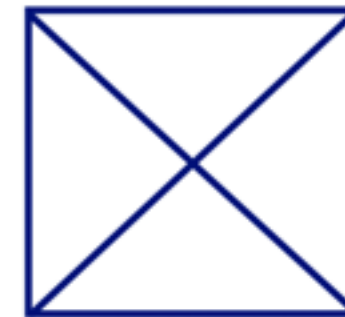
Avoiding Instability

- No general solution to avoid instability for complex mass-point systems.
- A smaller time step increases the chance for stability.
- A larger time step speeds up the simulation.
- Parameters and topology of the mass-point system, and external forces influence the stability of a system.
- Increasing damping does not always help.

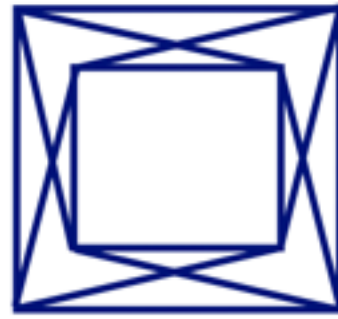
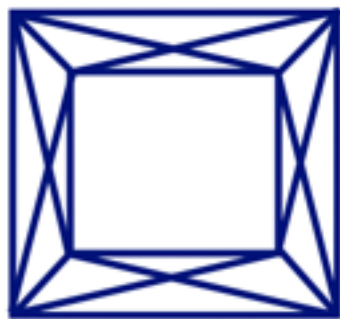
Topology and Stability

- Stable model topologies with respect to deformation

not stable



stable
but not
general

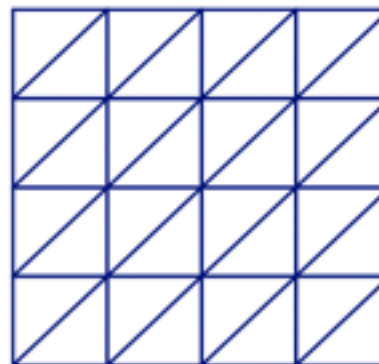




stable

can be generated automatically by copying the surface to an inner layer and connecting both – **layered model**

in the extreme case, consider the inner layer to be just a point

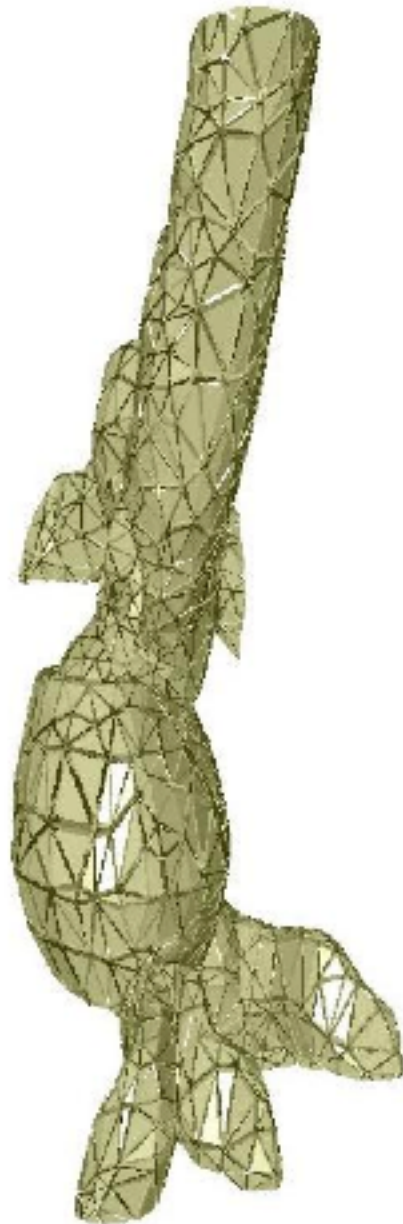
- Design problem



much more resistant in  direction than in  direction.

Volumetric Models - Tet Meshes

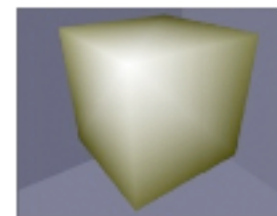
2949 mass points
10257 tets
15713 springs



1349 mass points
4562 tets
6888 springs

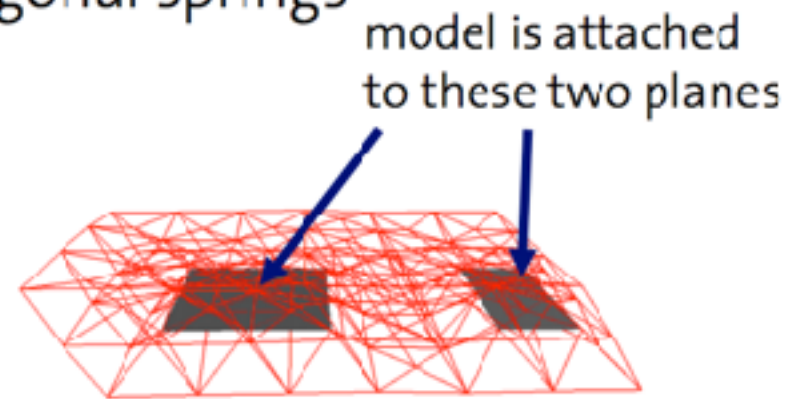
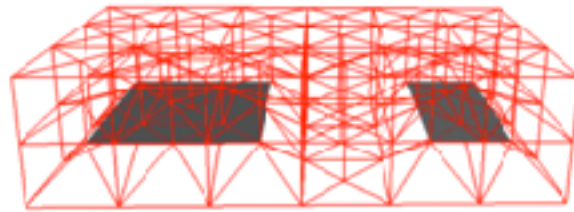


8 mass points
5 tets

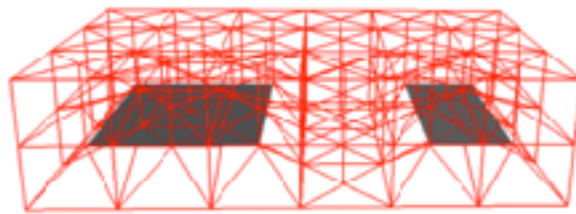


Topology Ambiguity Problem

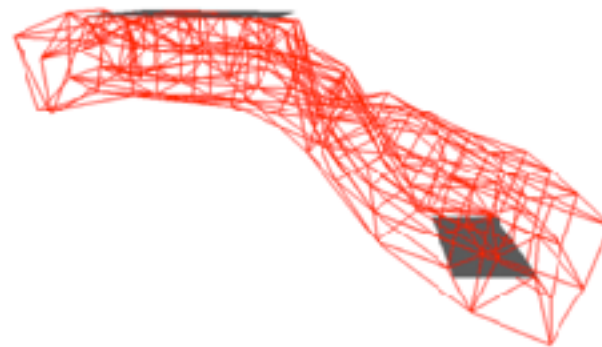
- Unappropriate topology without diagonal springs
- No force penalty for shearing



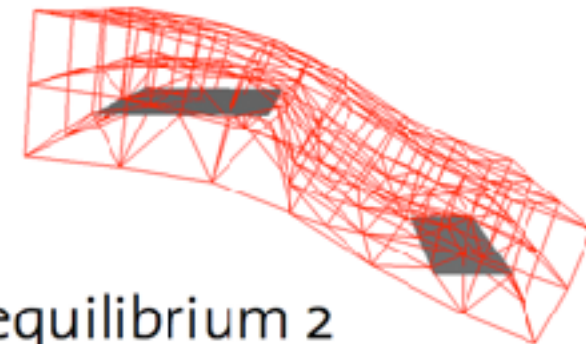
- Appropriate topology with diagonal springs
- However, self-collision problem, springs have no notion of volume



original



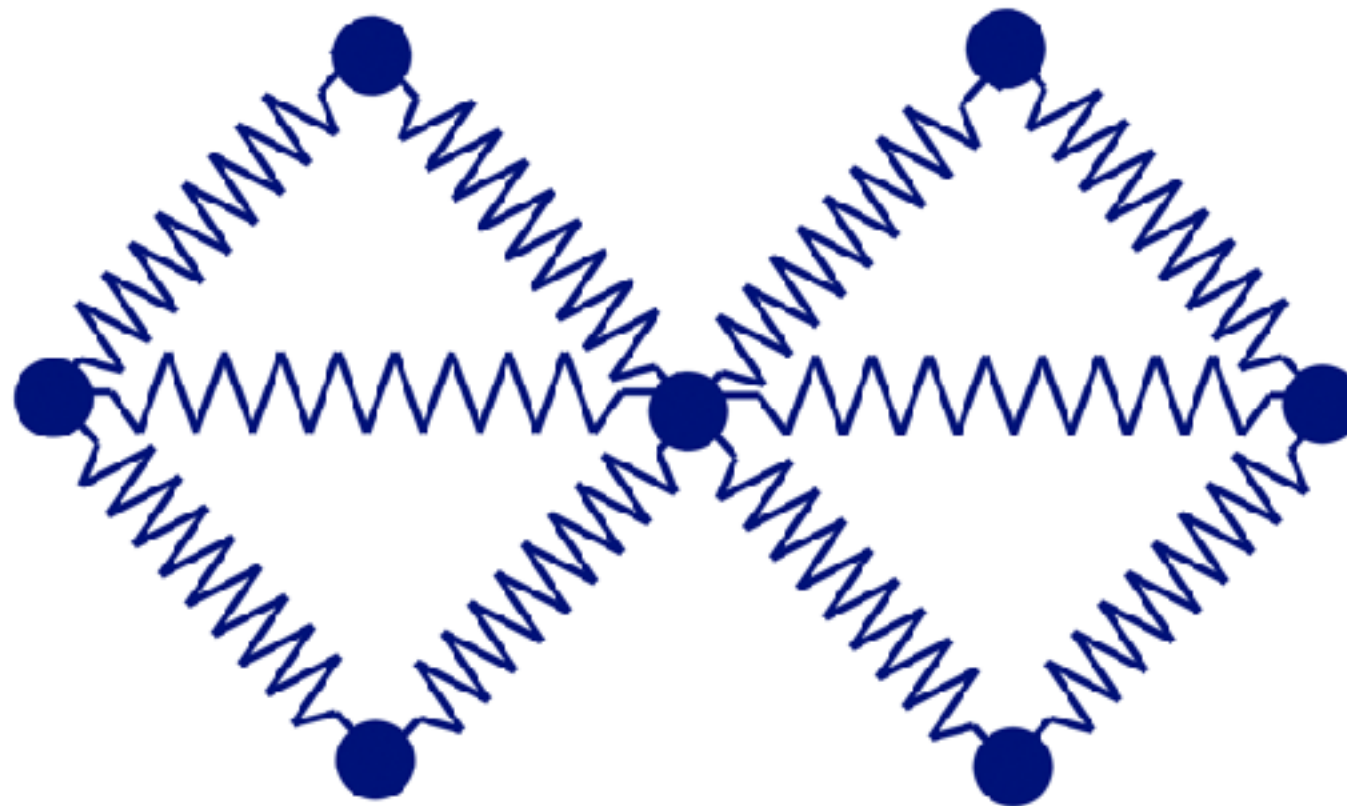
equilibrium 1



equilibrium 2

Cloth Forces

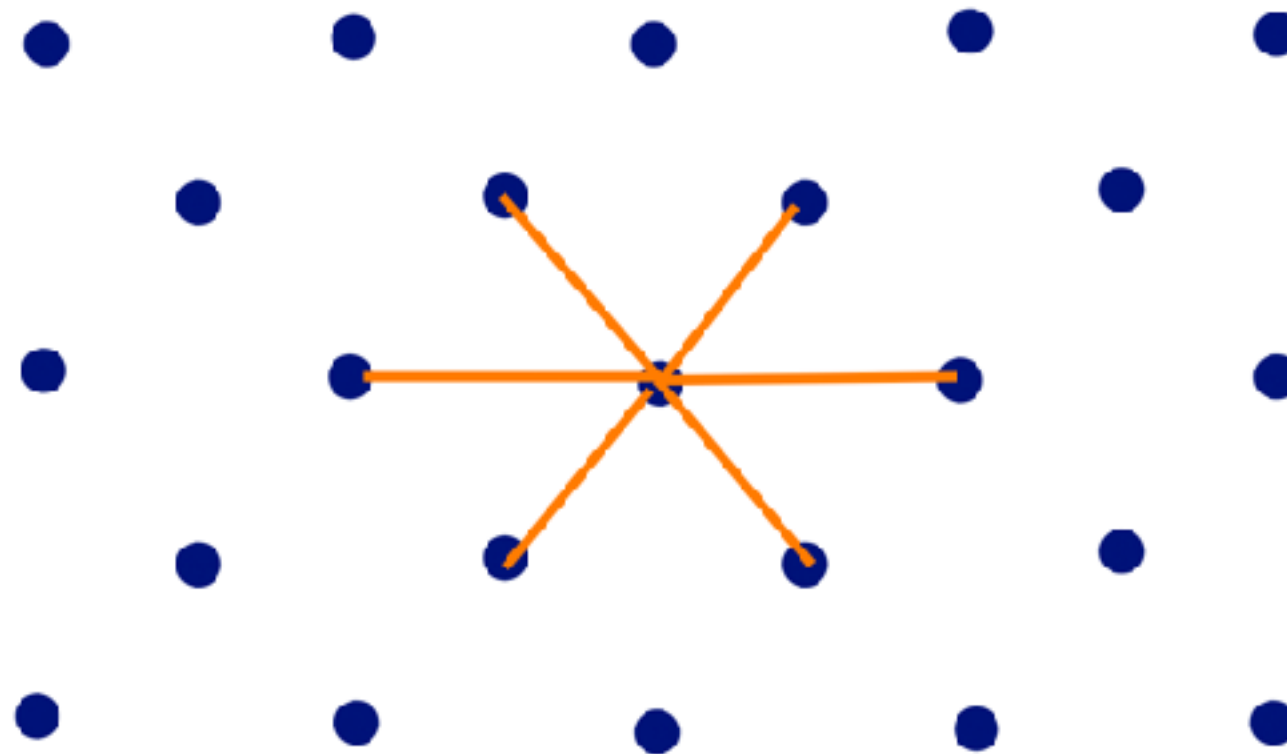
- Types of forces in cloth: **stretch**, **bending**, **shear**
- Bending cannot be modeled with a simple network of springs



Cloth Springs

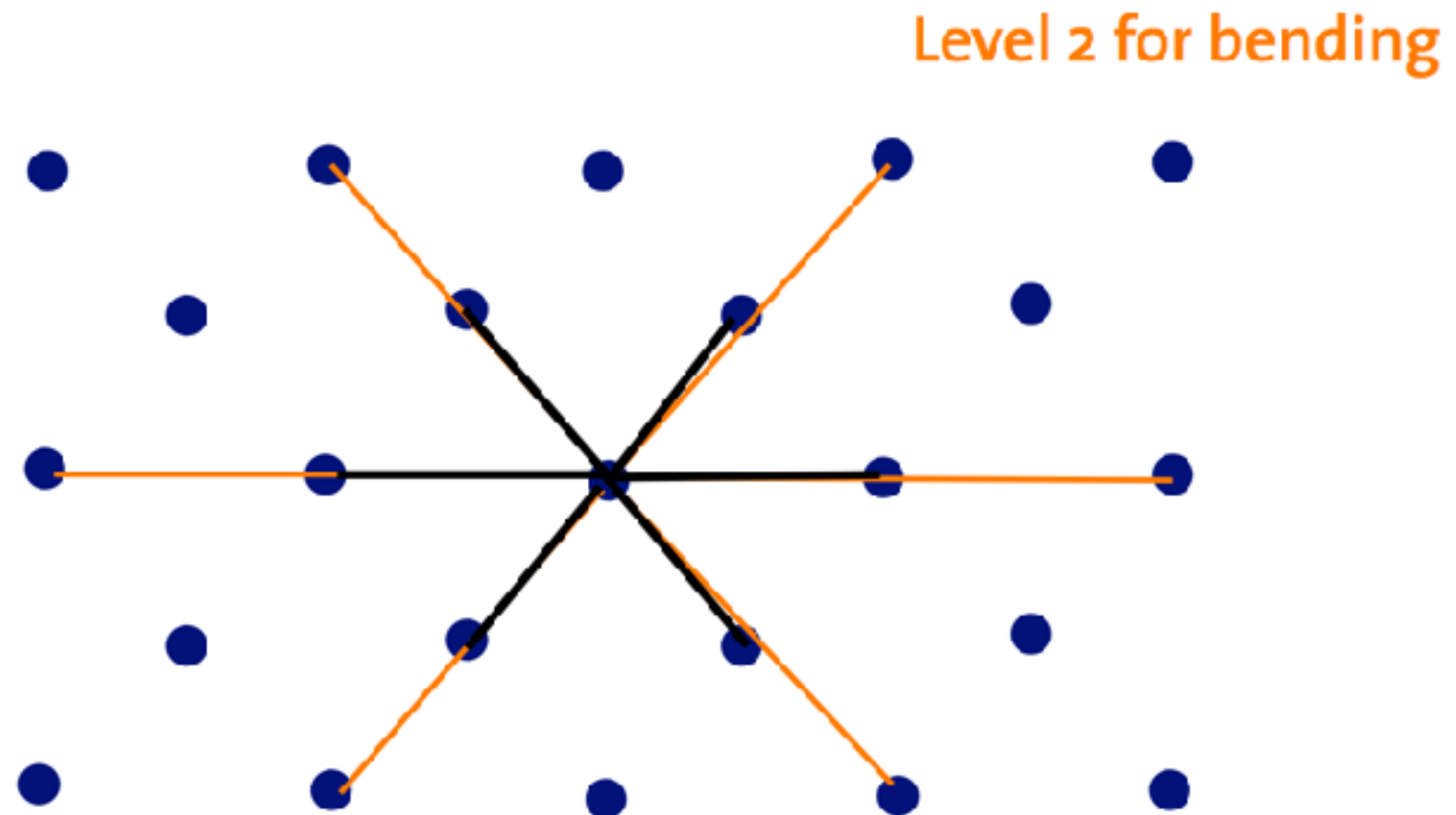
- Combine level-1 and level-2 springs

Level 1 for stretch

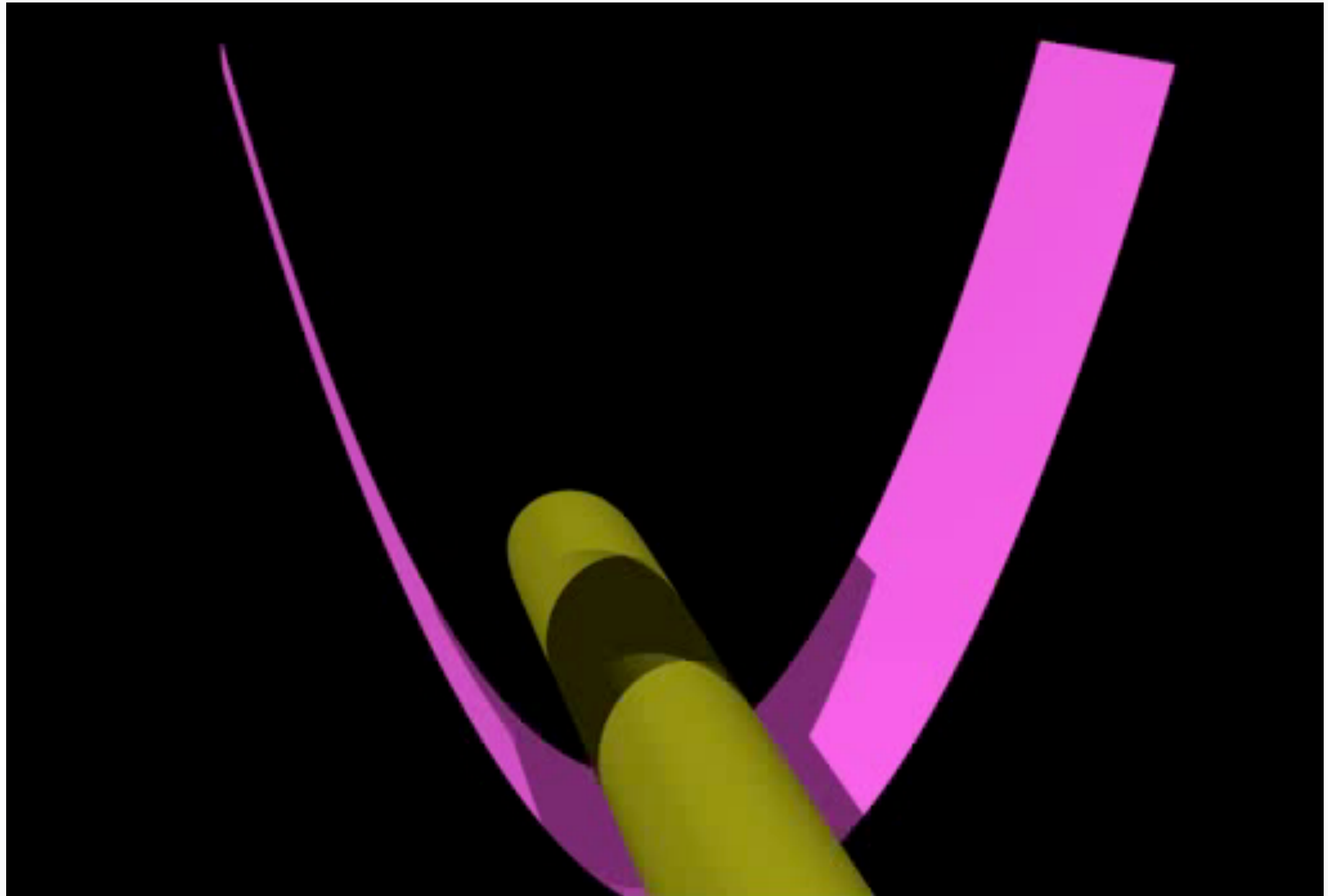


Cloth Springs

- Combine level-1 and level-2 springs



Cloth Springs



<http://cs420.hao-li.com>

Thanks!

